

# Field Effect Transistor - FET

Ian Scott  
ZL4NJ

[arb.xfm@gmail.com](mailto:arb.xfm@gmail.com)

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# Field Effect Transistor - FET

## Three Chapters

- **Chapter 1 - FET Evolution – 5 minutes**
- **Chapter 2 – Modern RF FET Fraternity – 10 minutes**
- **Chapter 3 - Example RF FET Circuits – 45 minutes**

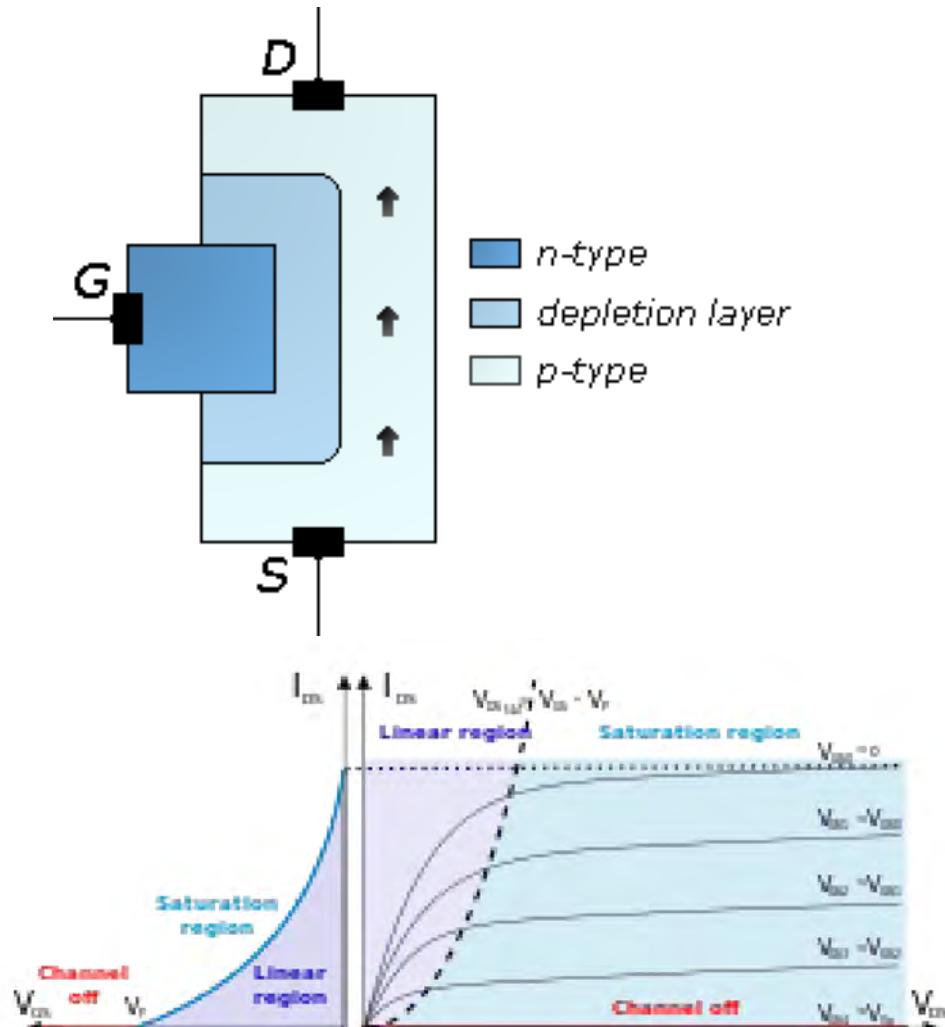
*Chapter 3a – Small Signal Low Noise Amplifiers (LNA)*

*Chapter 3b – Large Signal High Power Amplifiers (RFPA)*

*Chapter 3c – 23 cm 15 Watt LDMOS RFPA Design Journey*

# Field Effect Transistor – FET

## Chapter 1 - FET Evolution



- JFET Theory Patented by Julius Lilienfeld during 1920~1930
- However, JFET fabrication was Impossible until adequately pure silicon became available circa 1955, following silicon BJT
- Depletion Mode, Normally On

# Field Effect Transistor – FET

## Chapter 1 - FET Evolution

- First Junction Field Effect

Transistors (JFET) Resembled

Earliest Junction Bipolar

Transistors (BJT) Physical

Construction

# Field Effect Transistor – FET

## Chapter 1 - FET Evolution

- At this time, the JFET was considered to be the first “solid state valve”
- *Although not strictly accurate, the JFET was coined to be “voltage operated” - a close cousin to the familiar vacuum tubes of the time*
- In comparison the BJT was equally coined to be “current operated”
- Early BJT had low  $H_{FE}$  and therefore low input impedance, so this distinction made some sense. Early  $H_{FE} < 50$ , modern  $H_{FE} > 500$
- However early JFET had low gain, low power, limited high frequency

Modern BJT AC analysis models use “transconductance”  $g_m \equiv \partial I_c / \partial V_{be}$

# Field Effect Transistor – FET

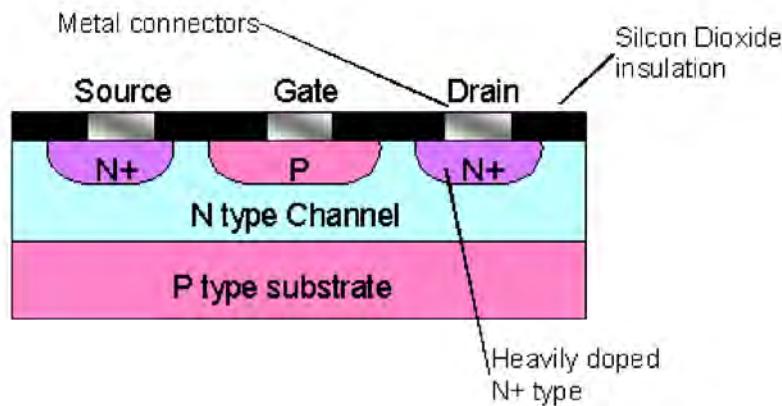
## Chapter 1 - FET Evolution

- Early JFET struggled to achieve  $g_m \sim 2 \text{ mA/Volt}$
- Some contemporary vacuum tubes could achieve  $g_m > 20 \text{ mA/Volt}$
- Early JFET were limited to audio frequencies
- In contrast, vacuum tubes where processing  $f > 500 \text{ MHz}!$
- As with early junction BJT, the limitation was in its construction
- The solution – *adopt the BJT planar fabrication process*

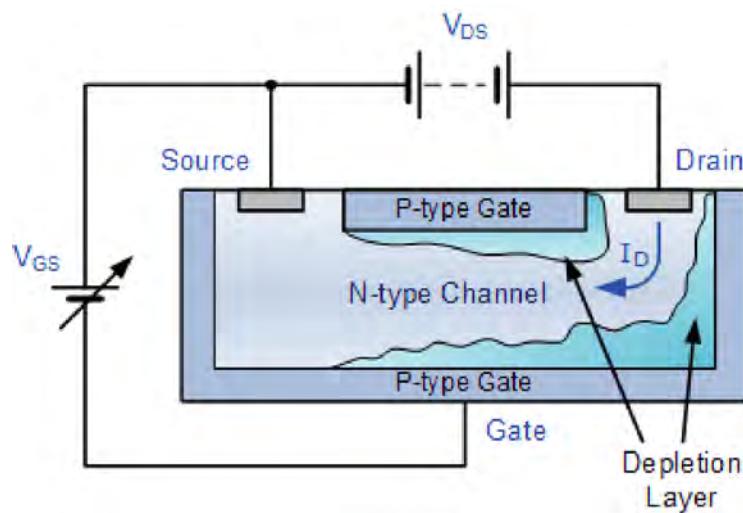
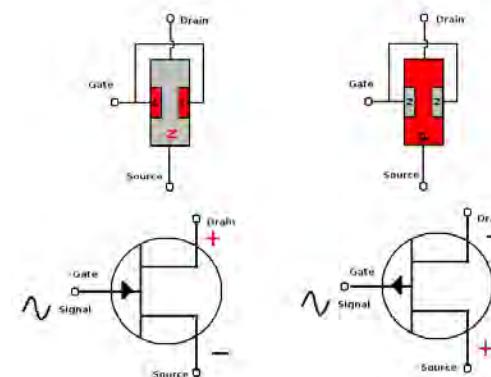
# Field Effect Transistor – FET

## Chapter 1 - FET Evolution

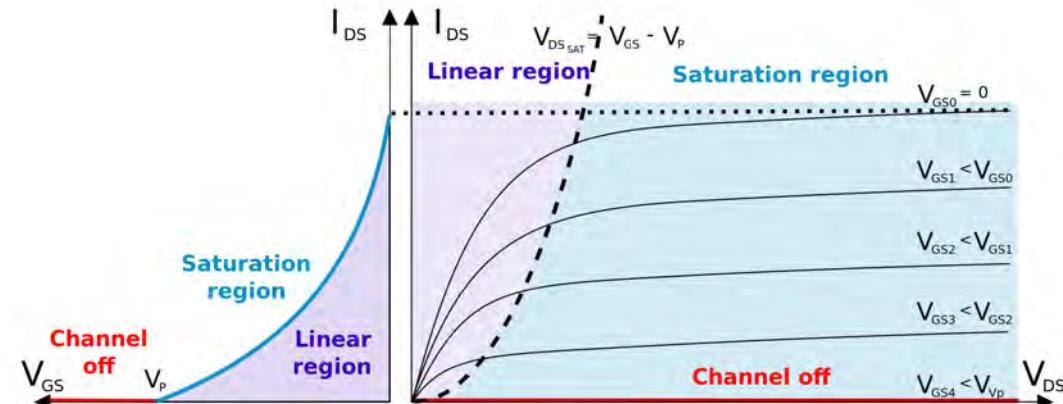
Note - modern planar construction



Note - same conceptual design!



Note – identical electrical characteristic



# Field Effect Transistor – FET

## Chapter 1 - FET Evolution

- JFET R&D investment downturn circa 1980
- However many popular JFET remain
- MPF102, 2N3819, 2N3823, 2N5459, J310, BF256
- Of these, the J310 die (originally U310 from Siliconix),  
was the pinnacle of high frequency JFET performance,

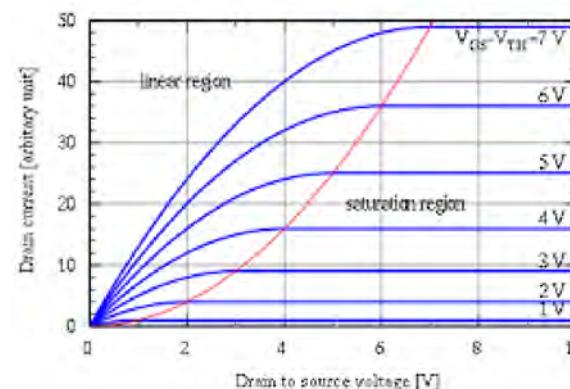
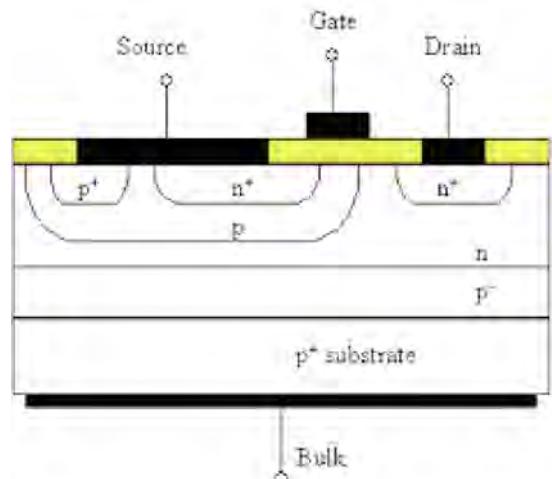
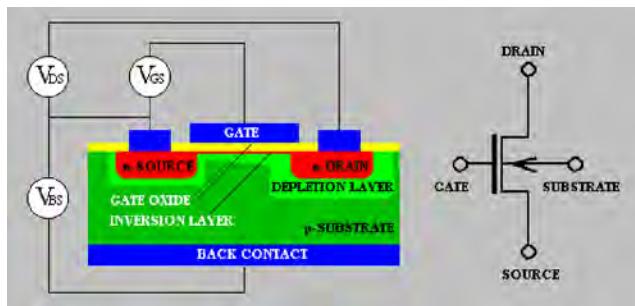
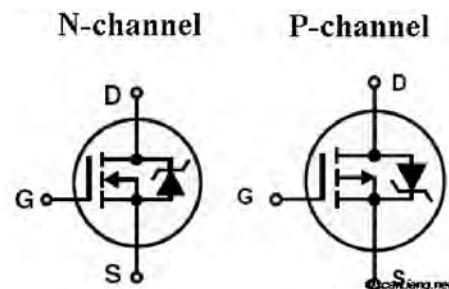
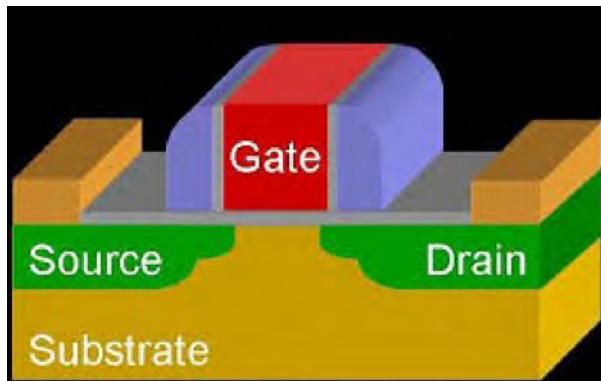
$$g_m \sim 20 \text{ to } 40 \frac{\text{mA}}{\text{Volt}}, f \sim 500 \text{ MHz}$$

- R&D funding targets MOSFET, IGBT, LDMOS, HEMT

# Field Effect Transistor – FET

## Chapter 1 - FET Evolution

Generic MOSFET construction



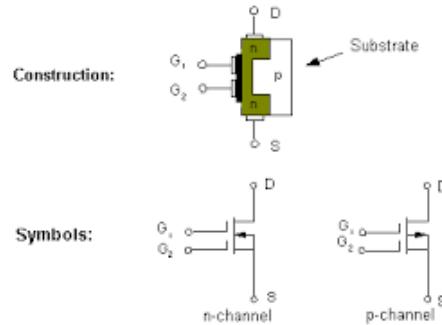
## Modern FET Types

- MOSFET
- IGBT
- LDMOS
- MESFET
- GaAsFET
- HEMT
- pHEMT



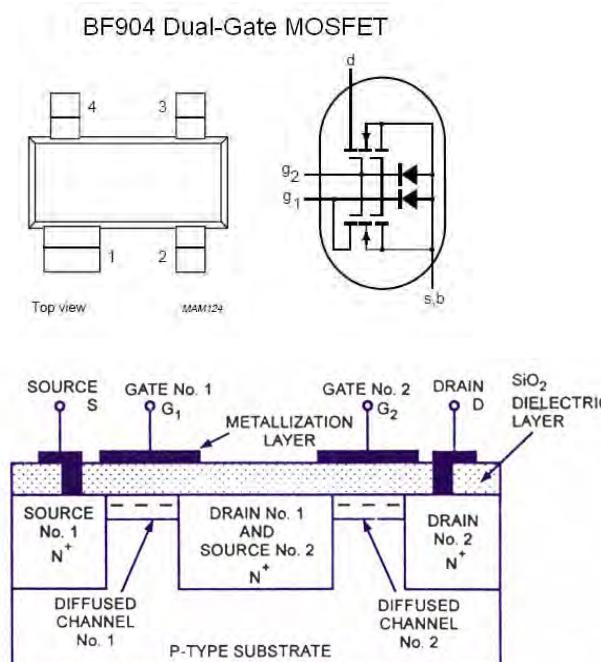
# Field Effect Transistor – FET

## Chapter 1 - FET Evolution

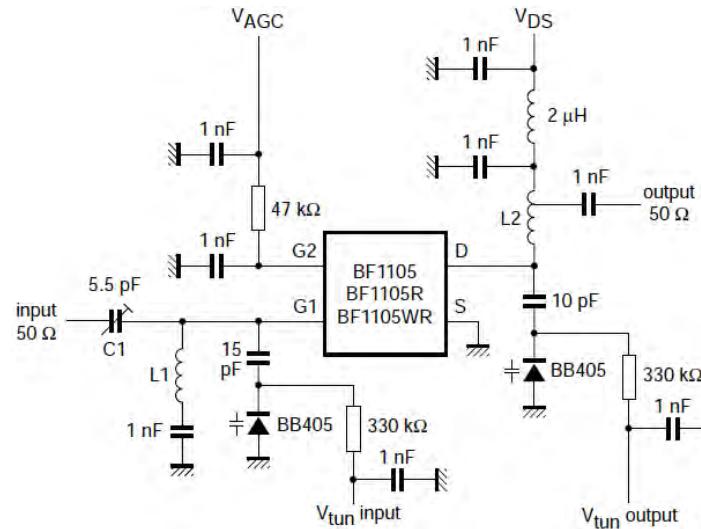


### Dual Gate MOSFET

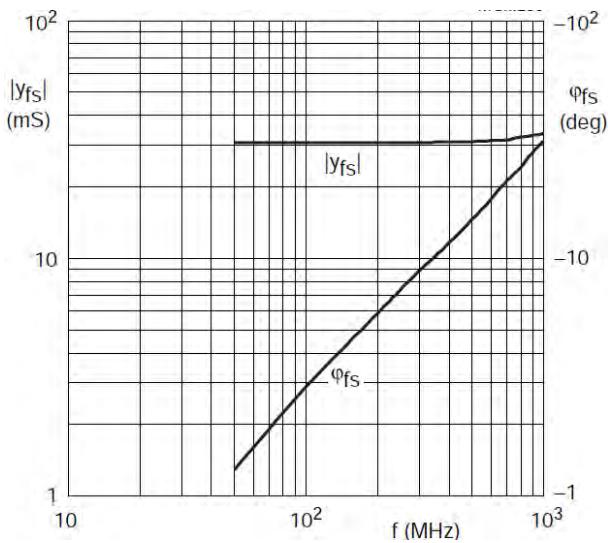
- Depletion and Enhancement modes available
- Very common in analog TV tuners as RF amplifiers
- Also well suited as mixers – BF1105 at 1296 MHz OK
- Typically cost less than \$NZ 1:00 (Digikey NZ)



### Infineon test circuit at 200 MHz



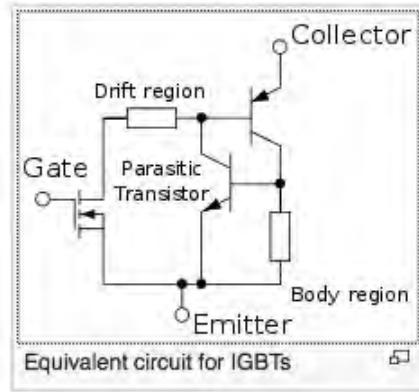
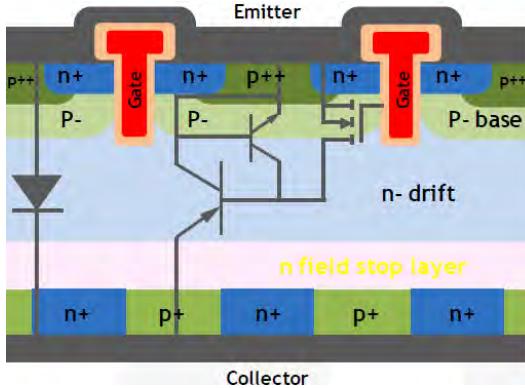
Suitable for 1,296 MHz!



From small signal LNA and mixers to high power...

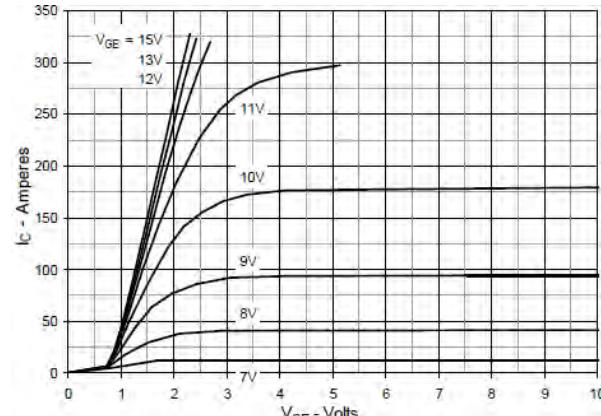
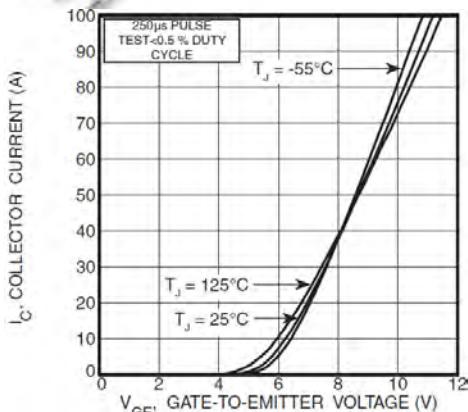
# Field Effect Transistor – FET

## Chapter 1 - FET Evolution



MOSFET input, common collector PNP BJT Output

**IXXK300N60B3**



How about integrating 2 MOSFET in series?

Insulated Gate Bipolar Transistor  
IGBT

- Ex. 600 V 300 Amp
- Switch to 100 kHz
- Speeds approach fast MOSFET
- Perhaps 80m RFPA

# Field Effect Transistor – FET

## Chapter 1 - FET Evolution - Summary

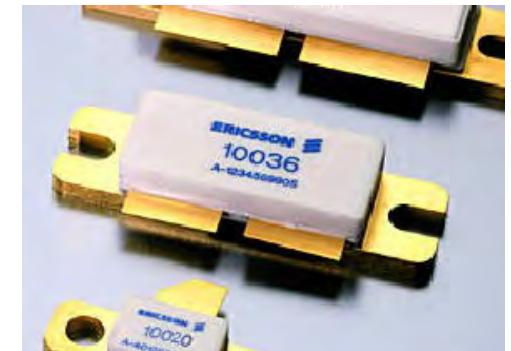
- Early Junction Field Effect Transistor (JFET)
- Depletion Mode, Low Gain, Logic Unfriendly
- Some improvement with Planar Process
- Superseded by Logic Friendly Enhancement MOSFET
- Subsequent IGBT, LDMOS, GaAsFET, GaN HEMT

# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity

Lateral Diffused MOS (LDMOS) – demonstrated 1969!

- Commercialized by Motorola – e.g. MRF181 1993
- Mature, > 10 years, Silicon, about \$NZ 1~2 per Watt
- High Power Transmitters, 1.5 kW VHF, 1 kW to 1 GHz
- High power amplification, Typical  $G_p \sim 17$  dB (50 x)



Gallium Arsenide FET (GaAsFET)

- Schottky Gate (same as MESFET, 1996) – Depletion Mode
- Low to Medium Power Linear Class A Microwave,  $V_s \leq 10$  V
- Current R&D Investment Not Visible – Legacy Technology



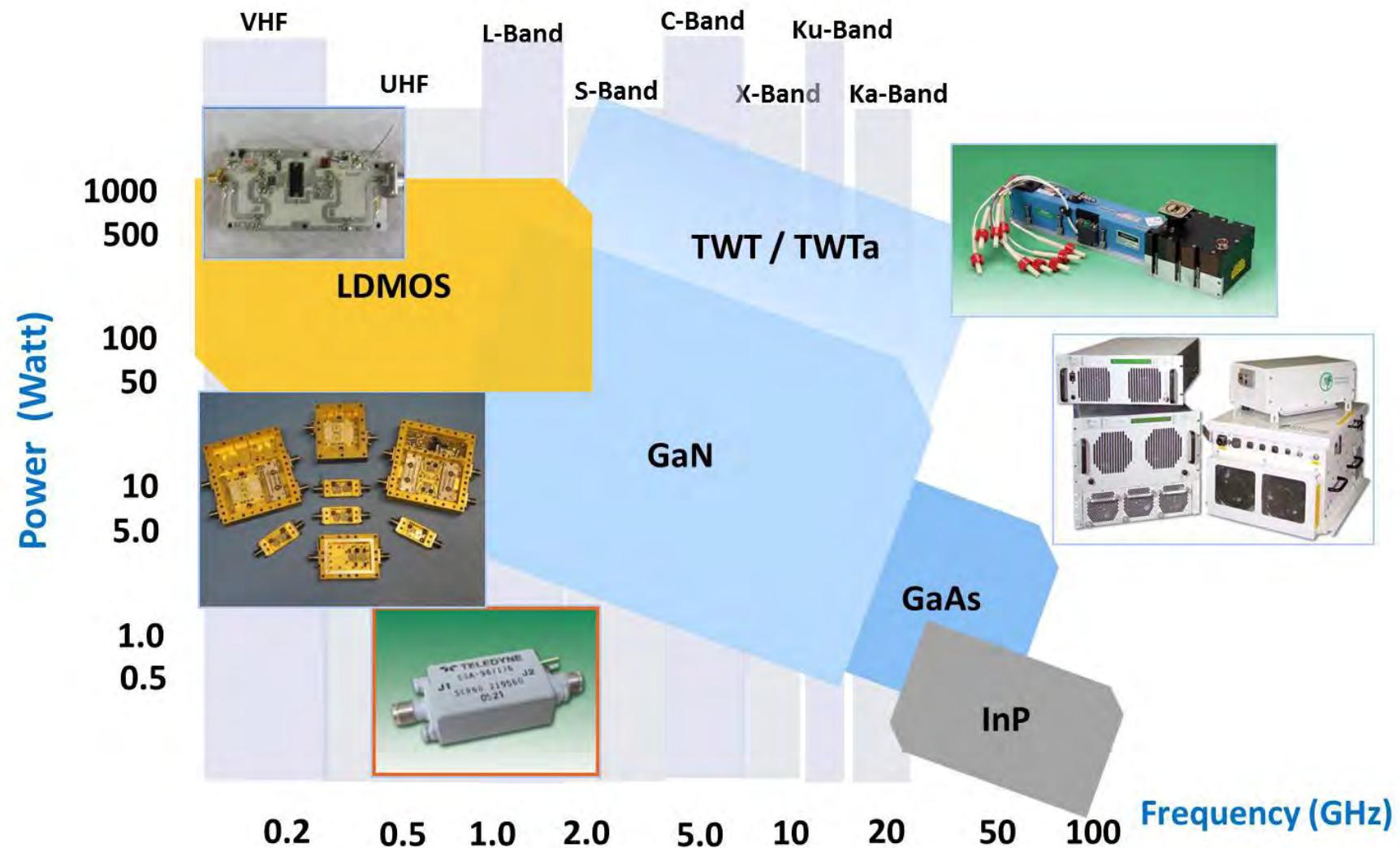
High Electron Mobility Transistor (HEMT)

- Current R&D Investment **Extremely Active**
- Medium to High Power (300W), ~ \$NZ 5 to 10 per Watt
- High Electron Mobility, ~ 5 x Silicon, Target DC To 6 GHz
- Small Signal LNA to 20 GHz, ~ \$NZ 2
- Very Recent – Faster Switch-mode Alternative to MOSFET



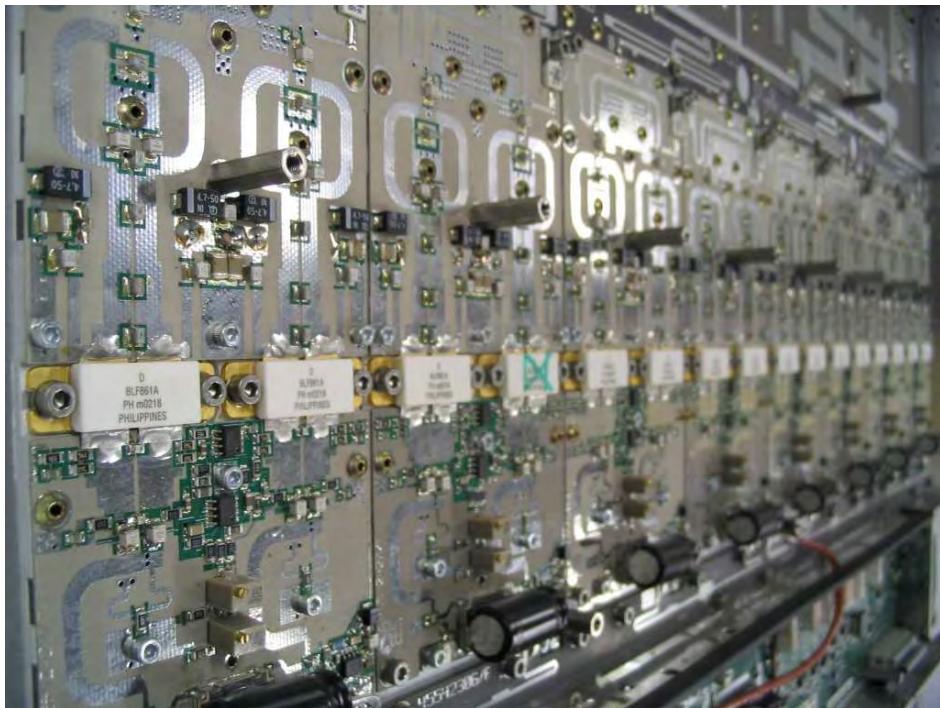
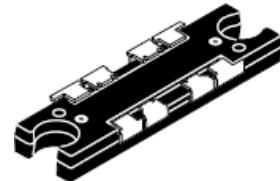
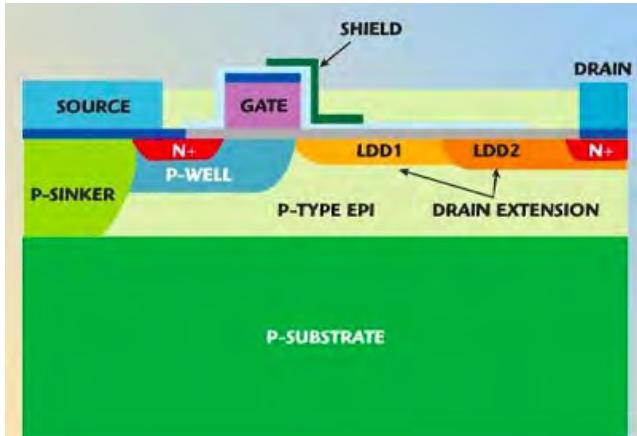
# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity

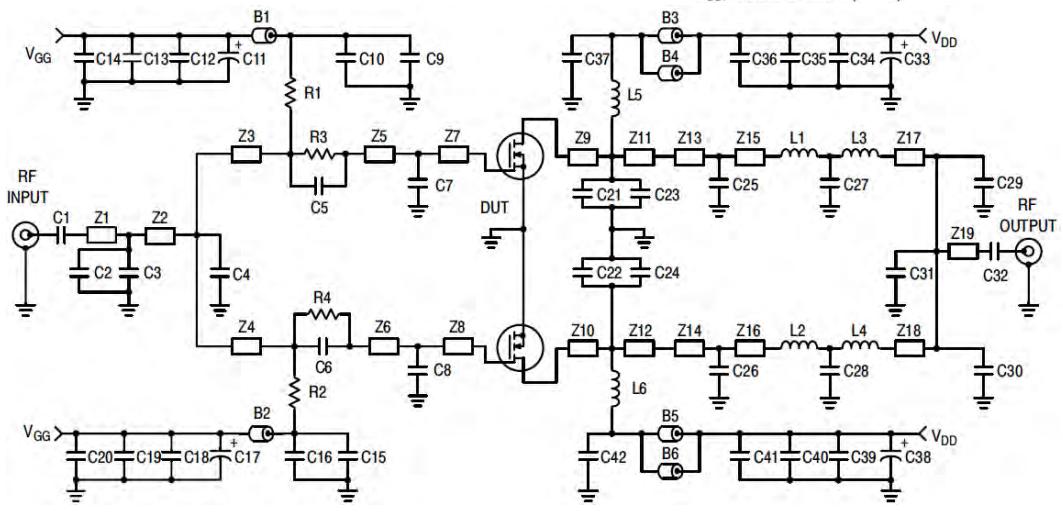
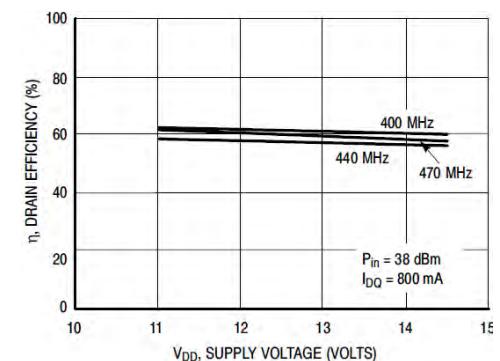
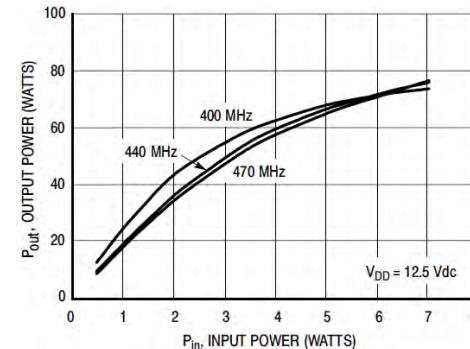


# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity

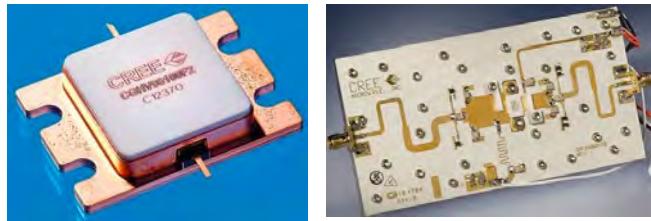


- Motorola Introduced LDMOS
- Immediately obsoleted BJT
- Upside down, heat from source
- MRF1570 70Watt \$NZ 70.41



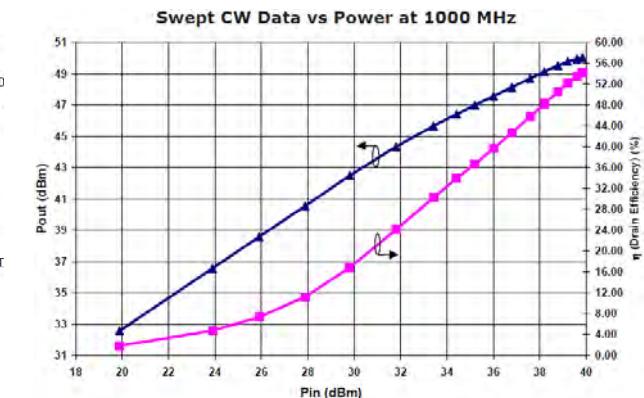
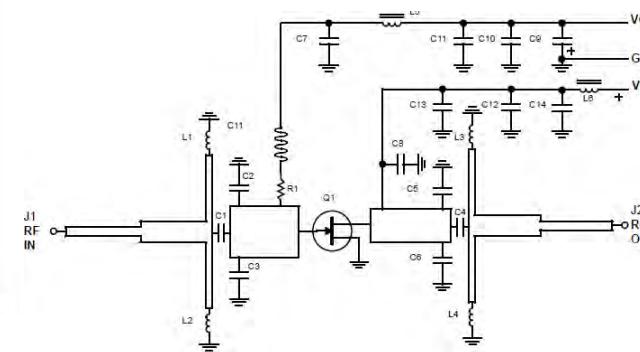
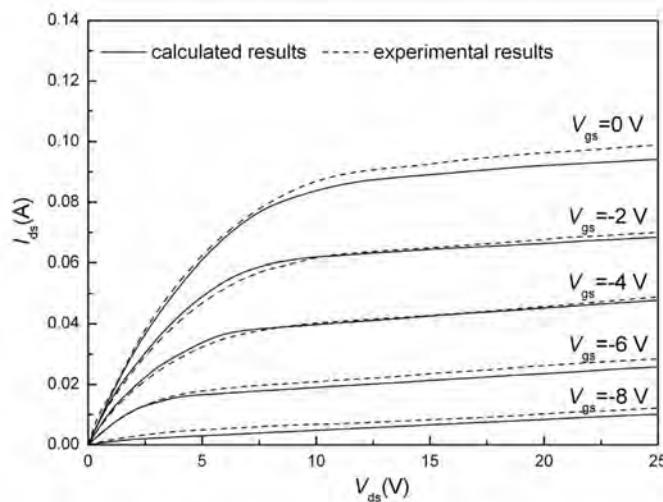
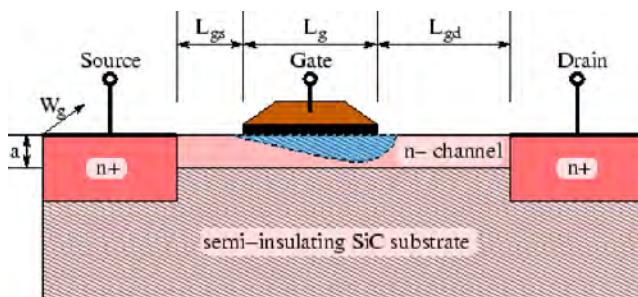
# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity



### MESFET

Metal Silicon Field Effect Transistor



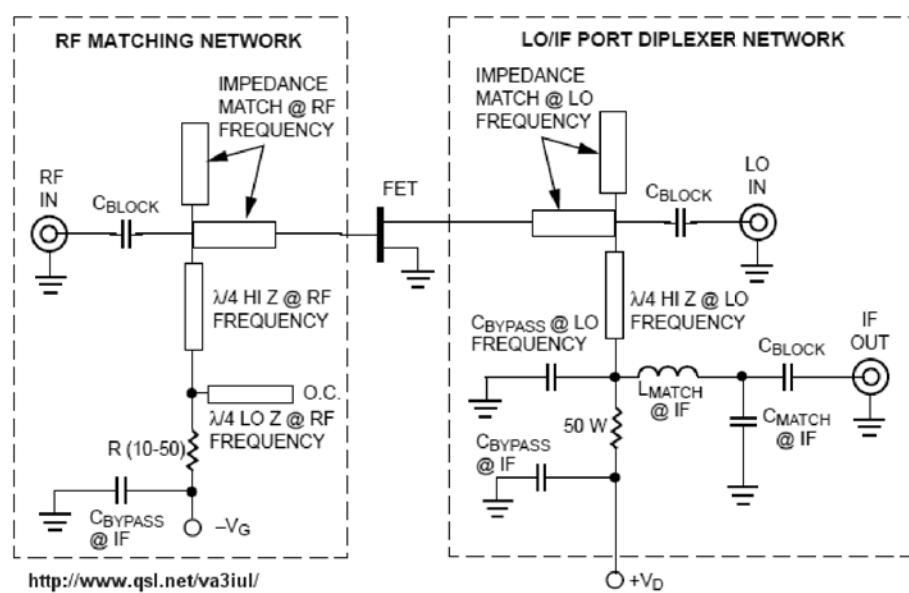
# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity

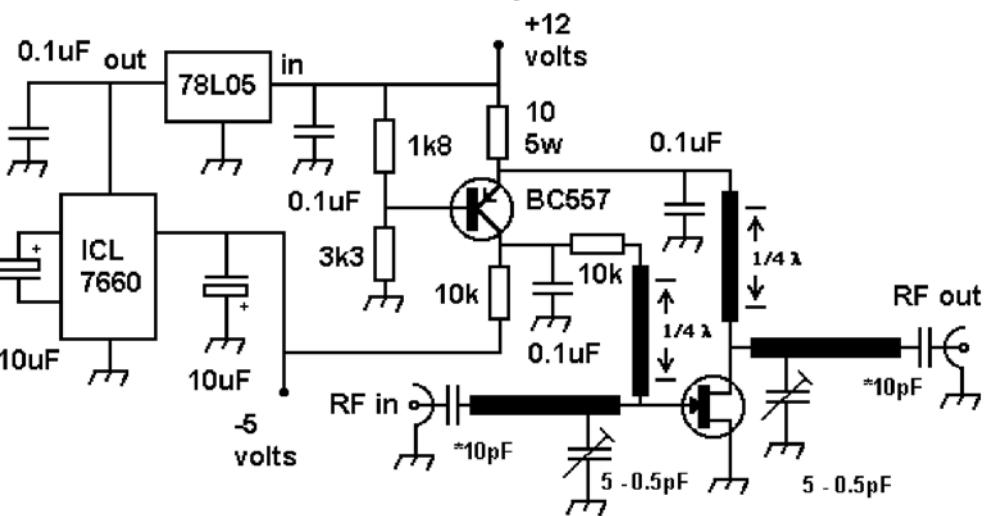


### GAsFET

- Depletion mode, always class A
- Medium power and small LNA
- Appears to receive little R&D



### 23cm low level linear amplifier



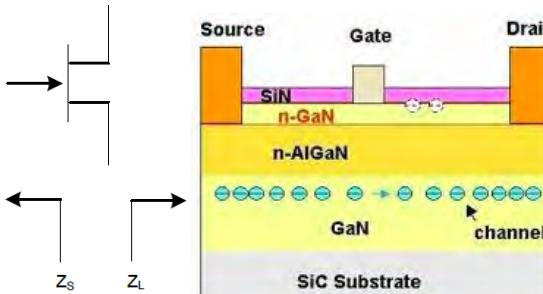
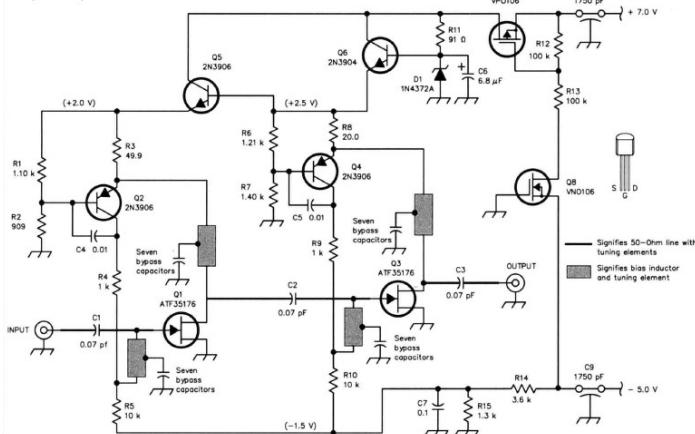
# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity



NPT2020 45 W 48 V  
DC–2.5 GHz HEMT  
\$151.29 Digikey NZ

<http://www.qsl.net/va3ul>



Load-Pull Performance:  $V_{DS} = 48$  V,  $I_{DQ} = 350$  mA,  $T_c = 25^\circ\text{C}$

Reference Plane at Device Leads, CW Drain Efficiency and Output Power Tradeoff Impedance

Frequency (MHz)	$Z_S$ ( $\Omega$ )	$Z_L$ ( $\Omega$ )	$P_{SAT}$ (W)	$G_{SS}$ (dB)	Drain Efficiency @ $P_{SAT}$ (%)
900	$1.1 + j0.7$	$7.3 + j5.5$	74	24	68
2000	$1.4 - j6.1$	$2.9 + j2.4$	65	17	68
2500	$1.5 - j7.6$	$2.3 + j0.6$	64	14	65

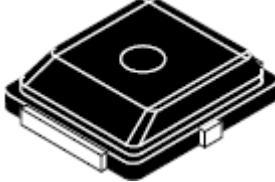
High Electron Mobility Transistor - HEMT

- Depletion mode FET
- Must sequence bias
- Gallium Nitride GaN
- Available,  $f > 6$  GHz
- Power up to 350 W
- Benign impedance
- Currently 2~3 \$/Watt

# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity

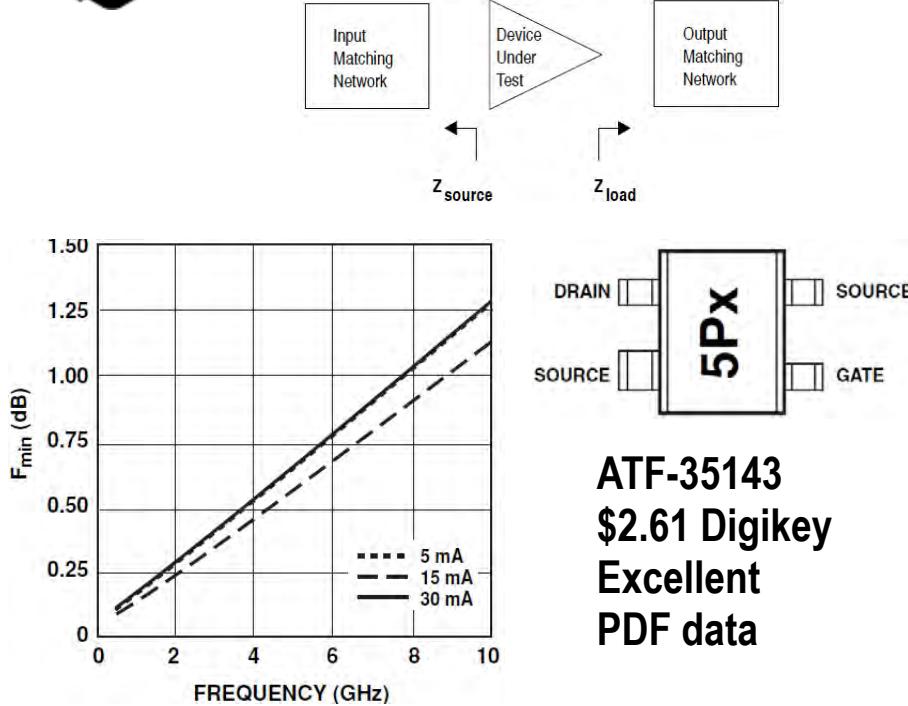
MRFG35010ANT1CT-ND pHEMT 3.55 GHz  
9 Watt 10 dB 12 V PLD-1.5 \$62.49, GaAs HEMT



$f$ MHz	$Z_{\text{source}}$ $\Omega$	$Z_{\text{load}}$ $\Omega$
3550	4.0 - j22.6	4.5 - j15.3

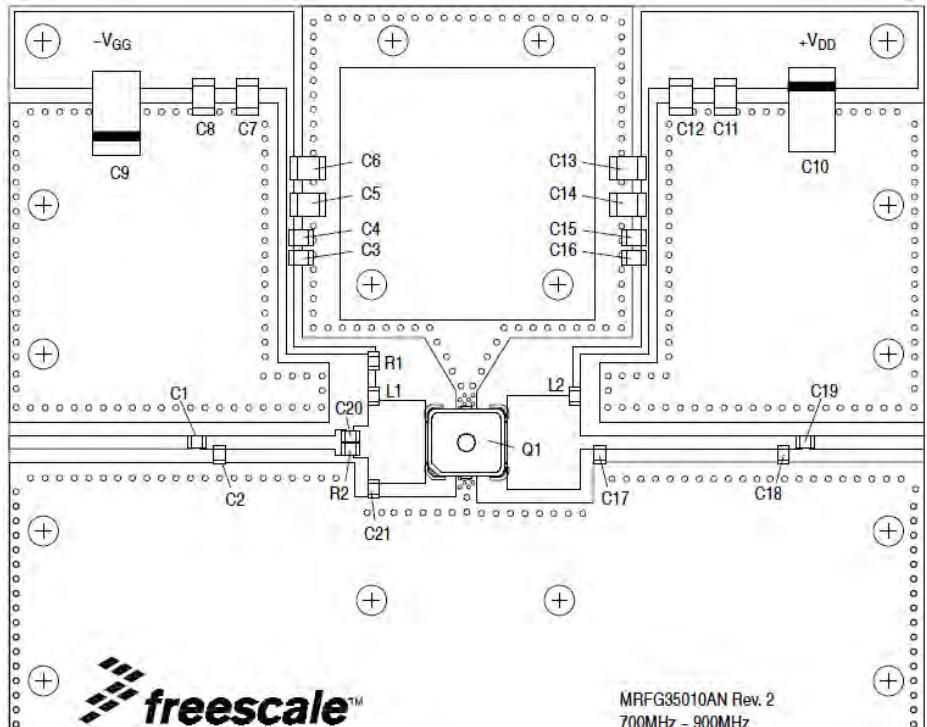
$Z_{\text{source}}$  = Test circuit impedance as measured from gate to ground.

$Z_{\text{load}}$  = Test circuit impedance as measured from drain to ground.



### Pseudomorphic HEMT - pHEMT

- LNA and Medium Power RFPA
- MRFG35010 z-Data is minimal
- ATF-35143 Avago z-Data is excellent
- Note – NF is inferred from PCB loss!



# Field Effect Transistor – FET

## Chapter 2 – The RF FET Fraternity - Summary

- LDMOS from Motorola, 1 kW to 1 GHz, Mature
- Higher Frequency Motivation – Early MESFET
- Close Cousin – GaAsFET – Medium Power - Class A
- High Electron Mobility Transistor (HEMT) – GaN
- HEMT - Massive Current R&D Investment – 6 GHz +

# Field Effect Transistor – FET

## Chapter 3 – Example RF FET Circuits

*Chapter 3a – Small Signal Low Noise Amplifiers (LNA)*

*Chapter 3b – Large Signal High Power Amplifiers (RFPA)*

*Chapter 3c – 23 cm 15 Watt LDMOS RFPA Design Journey*

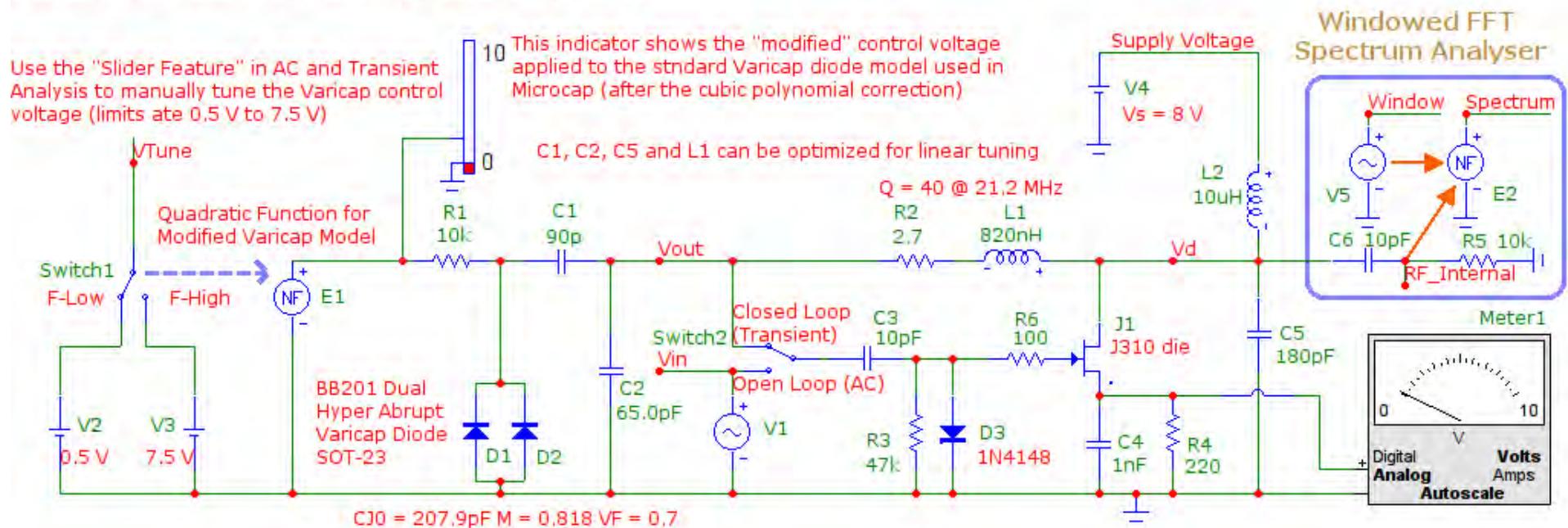
# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits

### 3a - Small Signal Low Noise Amplifiers (LNA)

Demonstration RF Voltage Controlled Oscillator (VCO) Simulation File by Ian Scott, 17 August 2013

Open loop (AC) and closed loop (Transient) analysis options are available (Switch2). Enhanced FFT Spectral analysis is provided by using a "Window Function" on the time domain data (V4, NF / E2). Two windows are used, data in the first window is ignored as this corresponds to start up oscillations. The second window processes signals once stable, steady state operation is achieved.

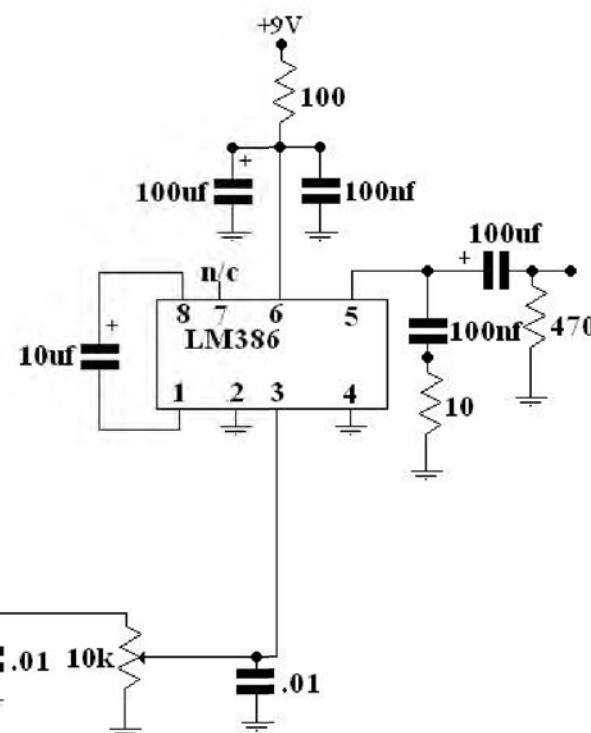
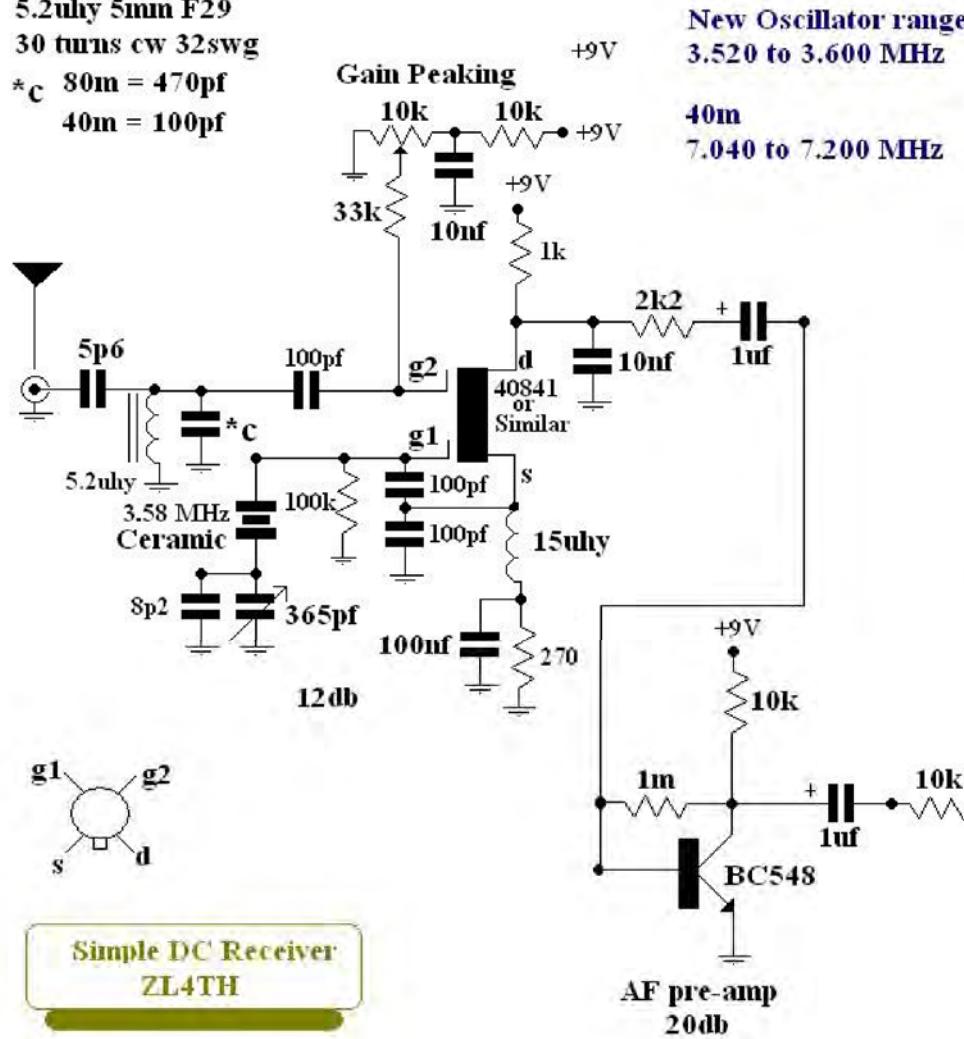


# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits

### 3a - Small Signal Low Noise Amplifiers (LNA)

5.2uhfy 5mm F29  
30 turns cw 32swg  
 $*C = 80\text{m} = 470\text{pf}$   
 $40\text{m} = 100\text{pf}$



# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits

### 3a - Small Signal Low Noise Amplifiers (LNA)

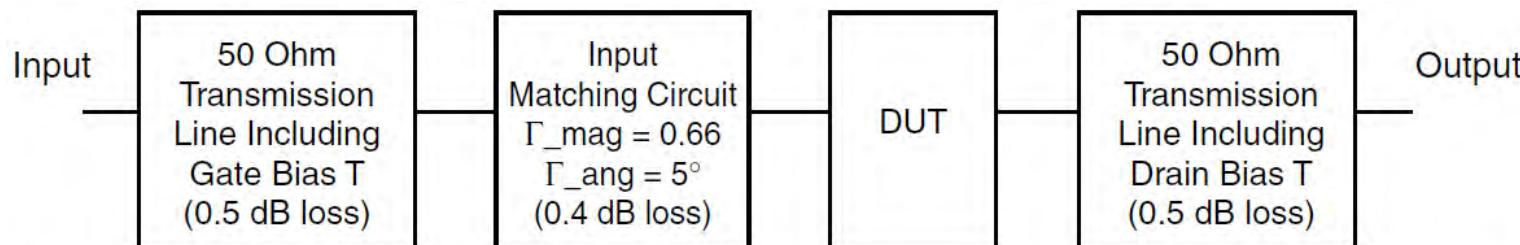
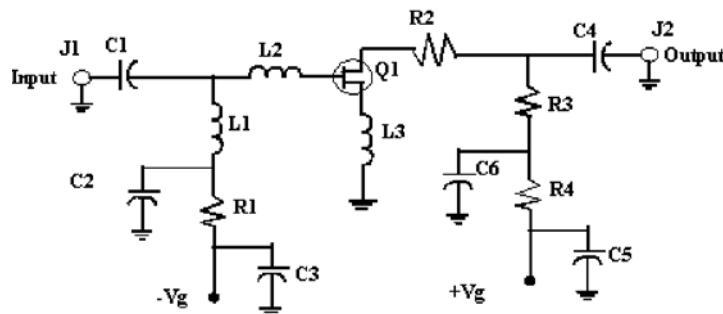
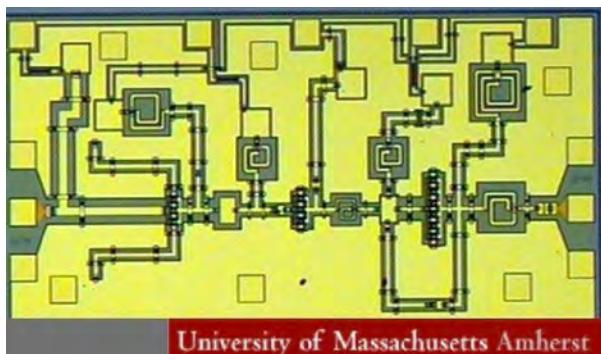


Figure 5. Block diagram of 2 GHz production test board used for Noise Figure, Associated Gain,  $P_{1\text{dB}}$ , and OIP3 measurements. This circuit represents a trade-off between an optimal noise match and a realizable match based on production test requirements. Circuit losses have been de-embedded from actual measurements.



- **Note** – Quoted NF is *Inferred* - Caveat Emptor!
- Typical pHEMT LNA – Needs Negative Gate Bias
- Best Input Noise Matching Only Uses Series  $L_2$



- Unencapsulated pHEMT Devices – Three Cascaded
- Spiral PCB Drain and Gate Bias Inductors
- Large Output Die – Low Power RFPA?

# Field Effect Transistor – FET

Chapter 3 - Example RF FET Circuits

*3b - Large Signal High Power Amplifiers (RFPA)*

## Radio Frequency Power Amplifiers

(RFPA)

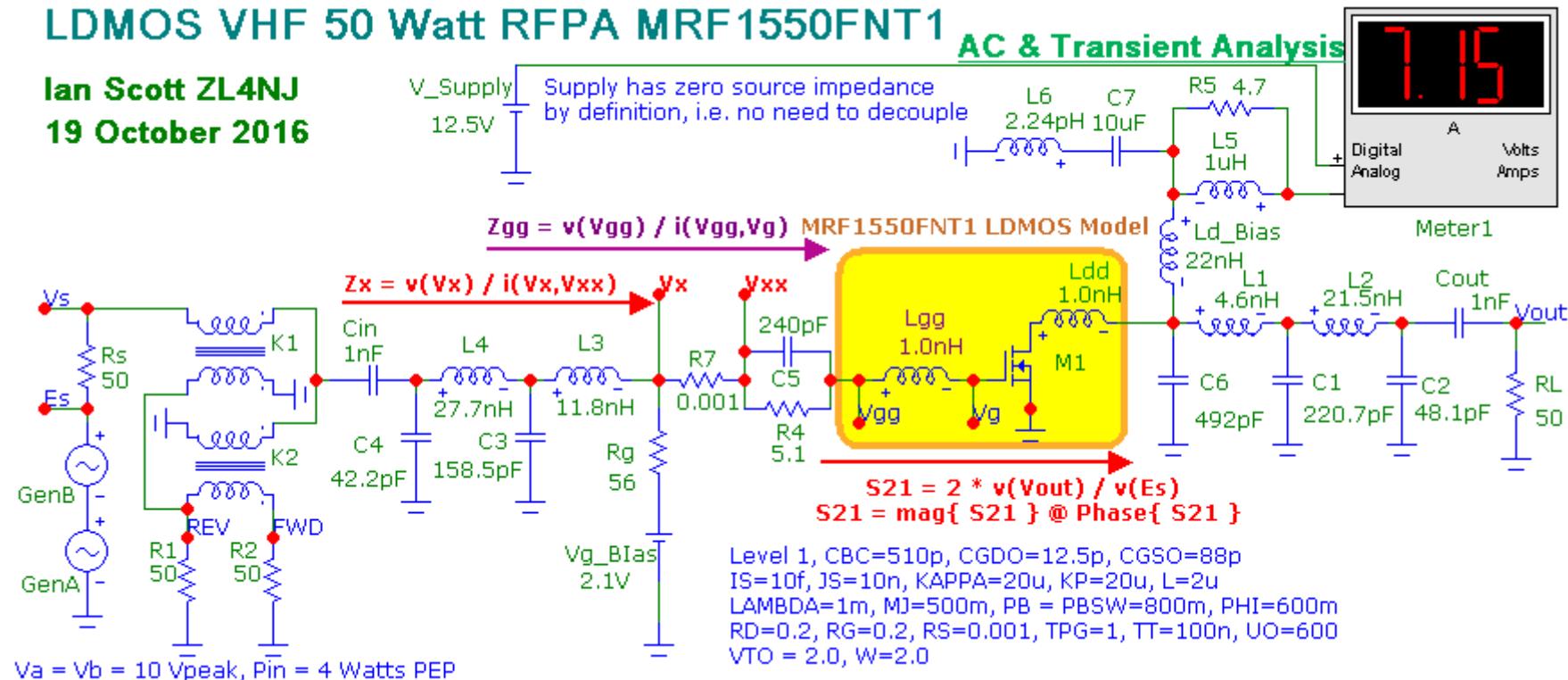
# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits

### 3b - Large Signal High Power Amplifiers (RFPA)

#### LDMOS VHF 50 Watt RFPA MRF1550FNT1

Ian Scott ZL4NJ  
19 October 2016



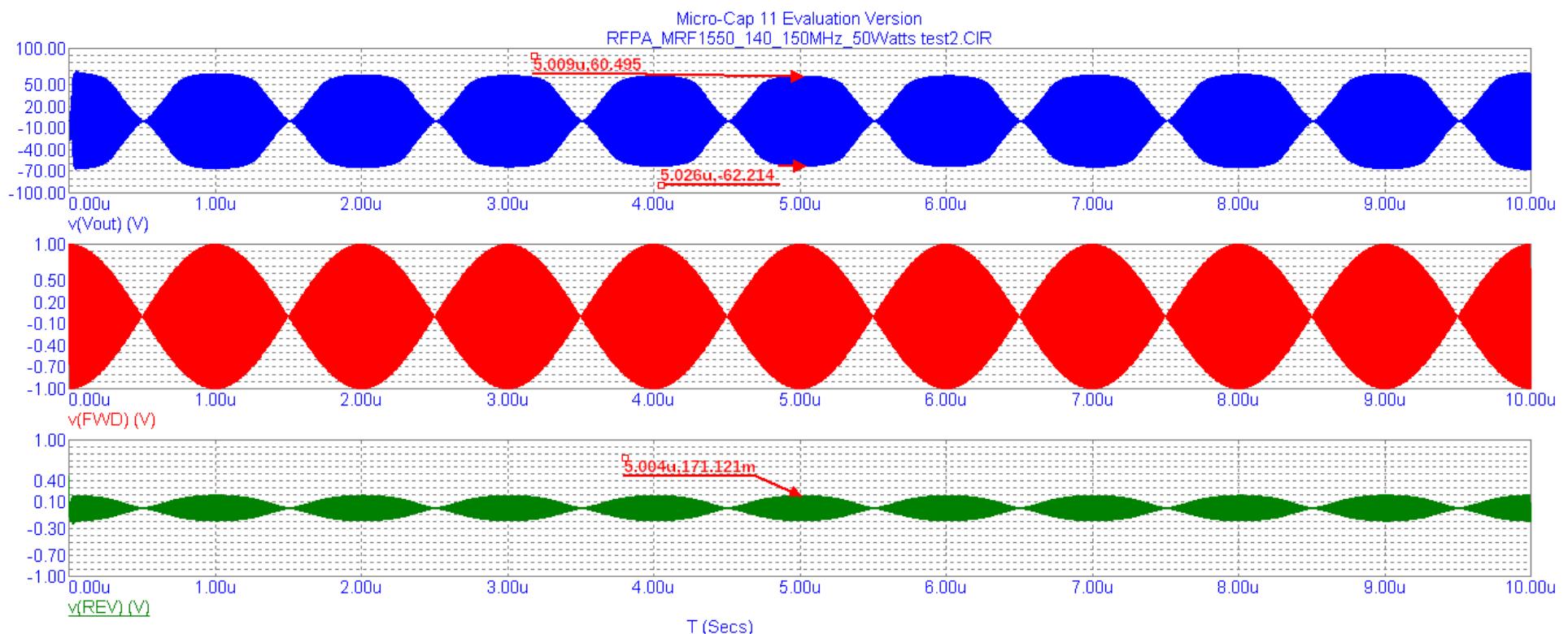
50 Watt VHF RF Power Amplifier using MRF1550 LDMOS Device

This topology is typical for all single ended LDMOS RFPA – lumped elements components are replaced with PCB micro-stripline at higher frequency and RF power

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits

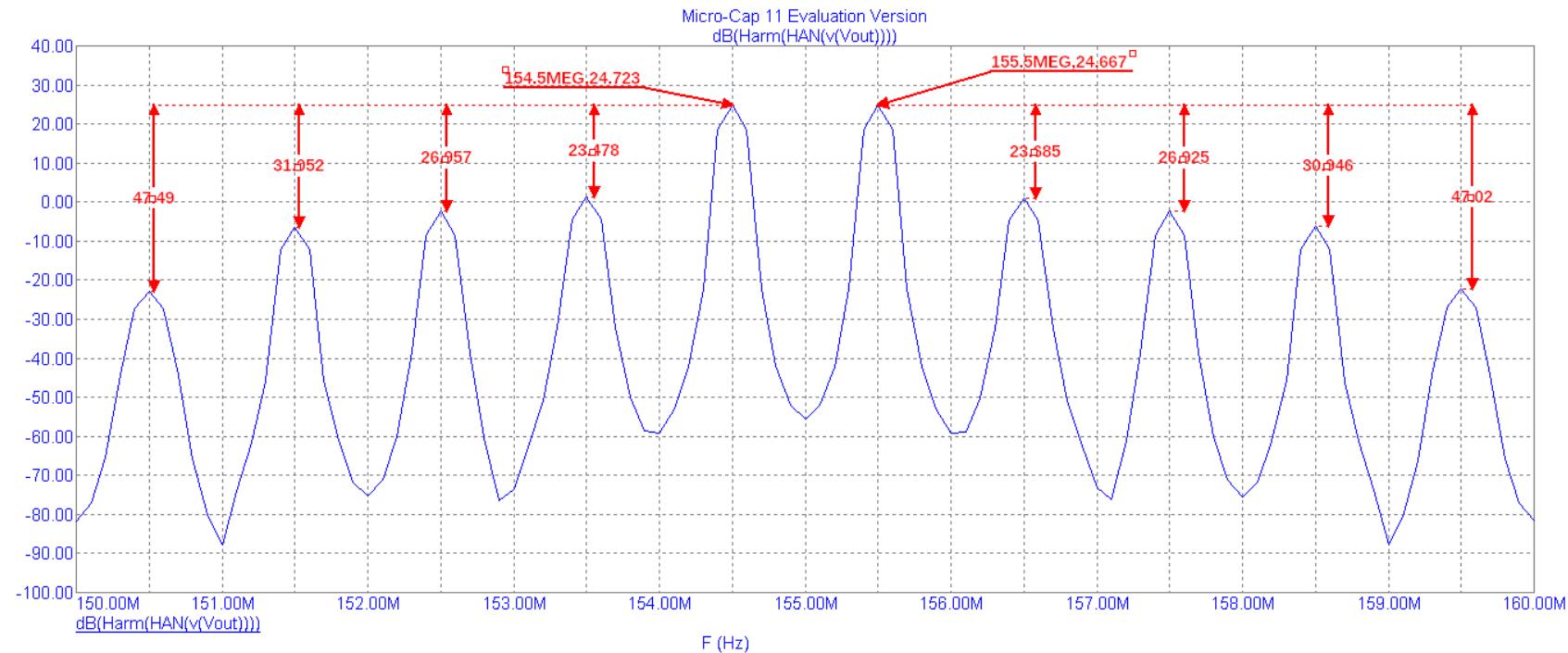
### 3b - Large Signal High Power Amplifiers (RFPA)



# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits

### 3b - Large Signal High Power Amplifiers (RFPA)



# Field Effect Transistor – FET

Chapter 3 - Example RF FET Circuits

*3c - 23 cm 15 Watt LDMOS RFPA Design Journey*

*1,250 – 1300 MHz 15 Watt LDMOS RFPA Design Journey*

- Applied RFPA Design Methodology
- Hypothetical 15 Watt 23 cm LDMOS RFPA
- Will use typical 870 MHz 15 Watt part
- Large Signal Impedance Data Extension from 500 – 1,000 MHz to 1,250 – 1,300 MHz

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

PD85015S-E 497-8296-5-ND 870MHz 15Watt 16dB 13.6V PowerSO-10RF \$30.66



Symbol	Test conditions	Min	Typ	Max	Unit
P3dB	$V_{DD} = 13.6 \text{ V}$ , $I_{DQ} = 150 \text{ mA}$ $f = 870 \text{ MHz}$	15	20	-	W
$G_P$	$V_{DD} = 13.6 \text{ V}$ , $I_{DQ} = 150 \text{ mA}$ , $P_{OUT} = 15 \text{ W}$ , $f = 870 \text{ MHz}$	16			dB
$h_D$	$V_{DD} = 13.6 \text{ V}$ , $I_{DQ} = 150 \text{ mA}$ , $P_{OUT} = P_{3dB}$ , $f = 870 \text{ MHz}$	60	70		%
Load mismatch	$V_{DD} = 17 \text{ V}$ , $I_{DQ} = 300 \text{ mA}$ , $P_{OUT} = 25 \text{ W}$ , $f = 870 \text{ MHz}$ All phase angles	20:1			VSWR

- Best Close Candidate – 23 cm amateur band has no commercial support
- PD85015S-E LDMOS Intended for  $f = 870 \text{ MHz}$  operation, just below 23 cm band
- Excellent initial power gain  $G_P = 16 \text{ dB}$ , fall  $-6 \text{ dB / octave}$ ,  $G_P \sim 16 - 3.5 = \underline{\text{12.5 dB}}$
- Note its extreme ruggedness – VSWR = 20:1 all phase angles, massive overdrive
- All LDMOS devices are equally suited for linear SSB as well CW FM

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

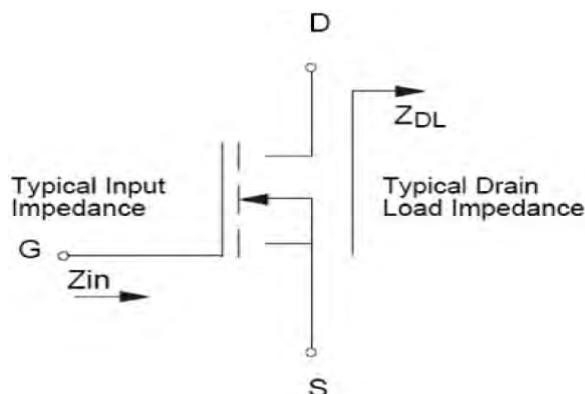


Table 7. Impedance data

Frequency	$Z_{IN} (\Omega)$	$Z_{DL} (\Omega)$
500 MHz	$0.536 - j 2.968$	$4.930 + j 1.083$
600 MHz	$0.557 - j 1.224$	$4.329 + j 0.811$
700 MHz	$0.595 + j 0.236$	$3.784 + j 0.429$
800 MHz	$0.651 + j 1.512$	$3.305 - j 0.031$
900 MHz	$0.708 + j 2.671$	$2.889 - j 0.542$
1000 MHz	$0.761 + j 3.759$	$2.534 - j 1.085$

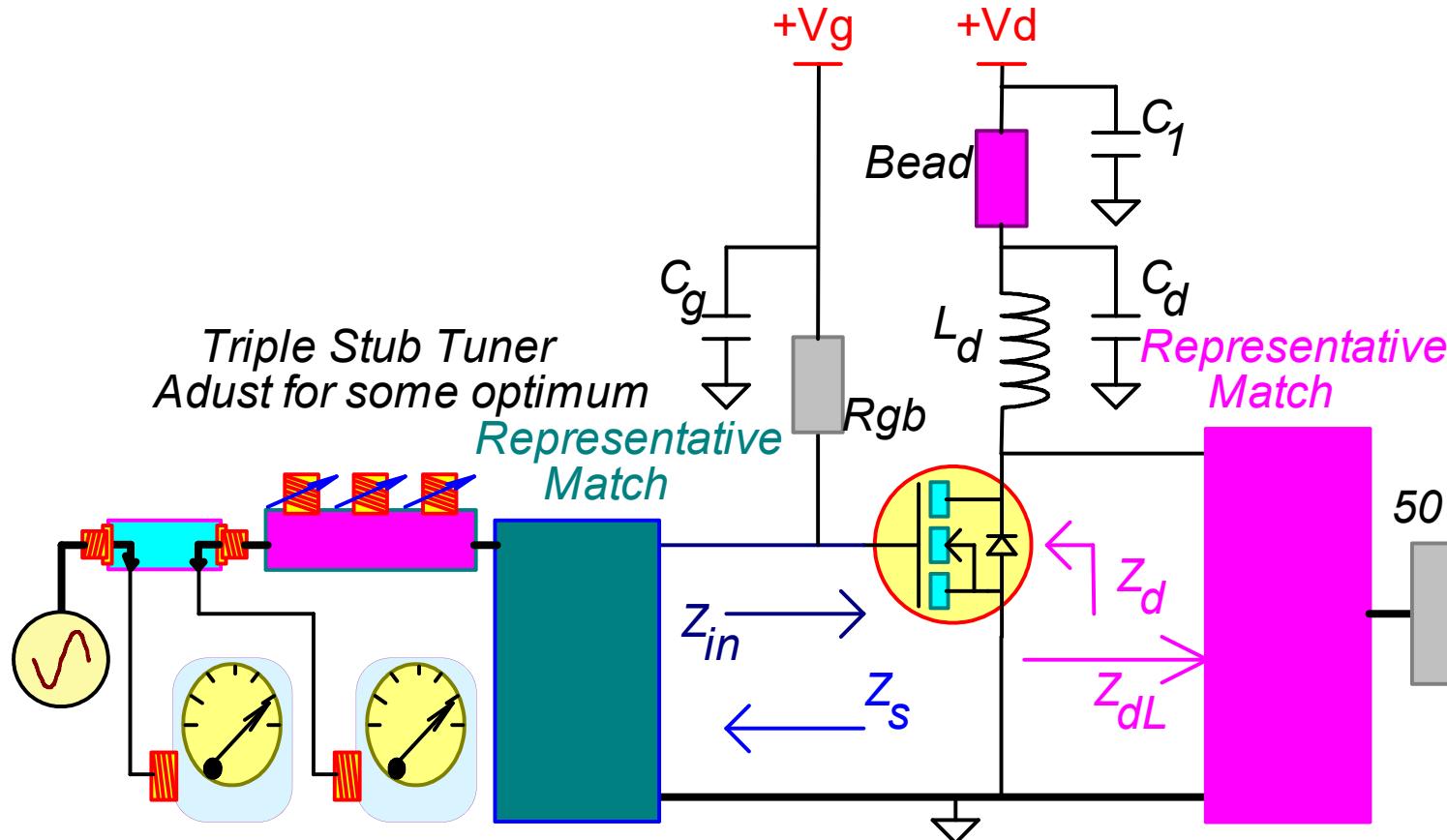
Note - impedance conventions can be defined at each terminal or by test fixture

- Large signal impedance data limited to 500 – 1,000 MHz
- However the general trend is smooth and gradual with  $f$
- The reactive component can be explained by lead inductance
- Can expect the input impedance  $Z_{in}$  to be high Q at 23 cm!

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

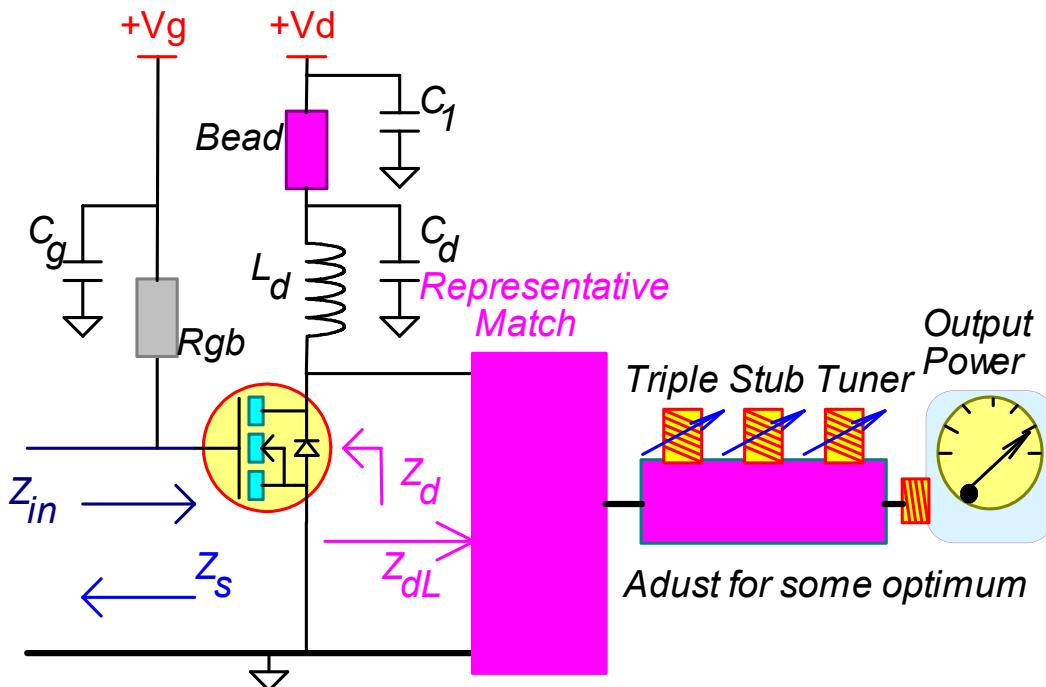
- Large signal device impedance use “load pull” measurement methodology
- Protects s-parameter measurement equipment from high RF Power levels
- Largely overcomes “harmonic interactions” - using representative matching networks



# Field Effect Transistor – FET

# **Chapter 3 - Example RF FET Circuits**

## ***3c - 23 cm 15 Watt LDMOS RFPA Design Journey***



- Output load pull characterization
  - Drain load  $Z_{dL}$  defines output power,  
not device  $Z_d$  (meaningless)
  - However “fictitious” conjugate impedances are used for designing suitable matching networks
  - Only for **lossless networks**  $Z_{in} = Z_s^*$

and  $Z_d = Z_{dL}^*$

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

$\alpha := \text{Find\_}\alpha(\text{Coefficients}, \Omega, Z_{in})$

$\beta := \text{Find\_}\alpha(\text{Coefficients}, \Omega, ZL)$

NewZin := Poly( $\alpha$ ,  $\Omega$ )

NewZin =

$$\begin{bmatrix} 0.536 - 2.968i \\ 0.557 - 1.224i \\ 0.596 + 0.236i \\ 0.651 + 1.512i \\ 0.708 + 2.671i \\ 0.761 + 3.759i \end{bmatrix}$$

$$Z_{in} = \begin{bmatrix} 0.536 - 2.968i \\ 0.557 - 1.224i \\ 0.596 + 0.236i \\ 0.651 + 1.512i \\ 0.708 + 2.671i \\ 0.761 + 3.759i \end{bmatrix}$$

NewZL := Poly( $\beta$ ,  $\Omega$ )

NewZL =

$$\begin{bmatrix} 4.93 + 1.083i \\ 4.329 + 0.811i \\ 3.784 + 0.429i \\ 3.305 - 0.031i \\ 2.889 - 0.542i \\ 2.534 - 1.085i \end{bmatrix}$$

$$ZL = \begin{bmatrix} 4.93 + 1.083i \\ 4.329 + 0.811i \\ 3.784 + 0.429i \\ 3.305 - 0.031i \\ 2.889 - 0.542i \\ 2.534 - 1.085i \end{bmatrix}$$

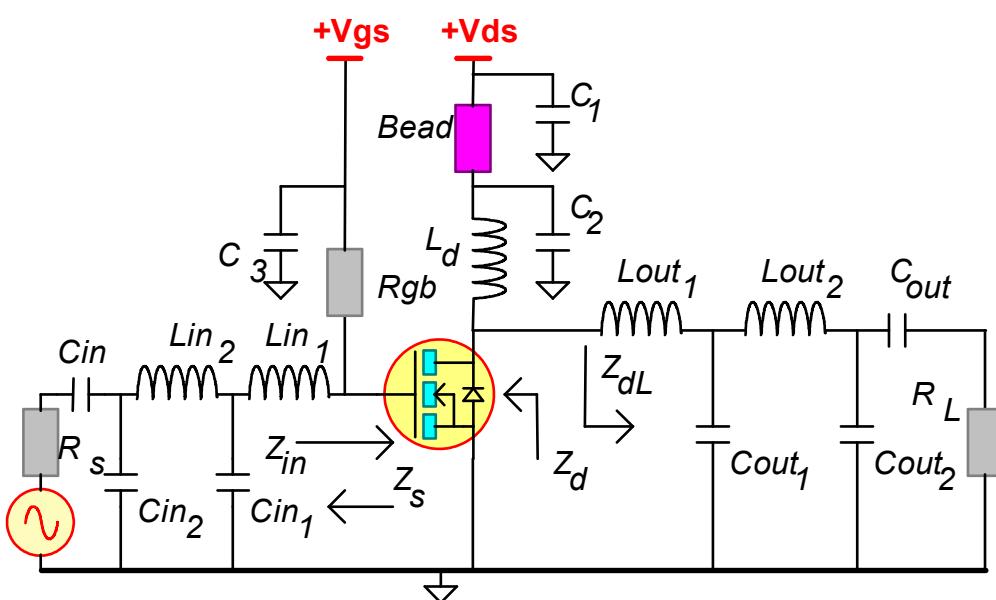
- Some Mathematics...
- Complex Polynomial
- z-Fit - Extrapolation
- Moore - Penrose
- Pseudo-matrix
- Inversion
- Singular Value
- Decomposition – SVD
- Excellent Test Cases

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

Frequency in GHz   Gate Impedance,  $\Omega$    Load Impedance,  $\Omega$

$$\frac{F}{1000} = \begin{bmatrix} 1.25 \\ 1.26 \\ 1.27 \\ 1.28 \\ 1.29 \\ 1.3 \end{bmatrix} \quad \text{NewZin} = \begin{bmatrix} 1.143 + 6.422i \\ 1.183 + 6.534i \\ 1.225 + 6.647i \\ 1.272 + 6.761i \\ 1.322 + 6.877i \\ 1.376 + 6.994i \end{bmatrix} \quad \text{NewZL} = \begin{bmatrix} 2.074 - 2.565i \\ 2.078 - 2.63i \\ 2.085 - 2.696i \\ 2.095 - 2.763i \\ 2.108 - 2.831i \\ 2.124 - 2.899i \end{bmatrix}$$



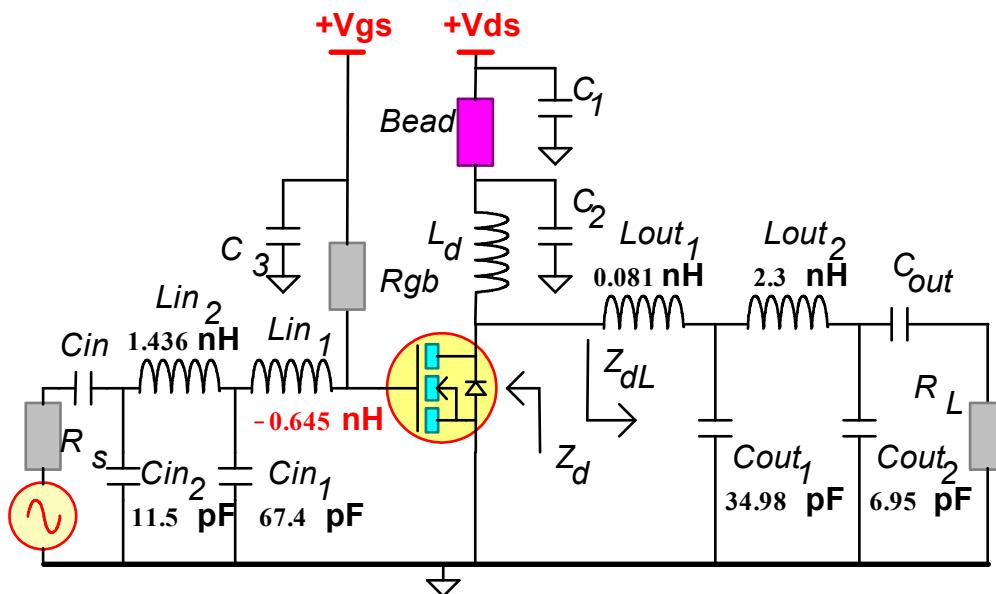
- Polynomial Prediction for 23 cm
- High  $Z_{in}$  reactance - “Q” (bad)
- Very Benign Load  $Z_{dL}$
- Use Conjugate  $Z_d \equiv Z_{dL}^*$  for Output Network Synthesis
- Prototype Test Circuit
- Will Use Lumped Element N = 4 Matching Networks
- Convert to PCB Microstripline Later

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

Lin1 = -0.645	nH	Lout1 = 0.081	nH
Cin1 = 67.352	pF	Cout1 = 34.981	pF
Lin2 = 1.436	nH	Lout2 = 2.358	nH
Cin2 = 11.502	pF	Cout2 = 6.95	pF

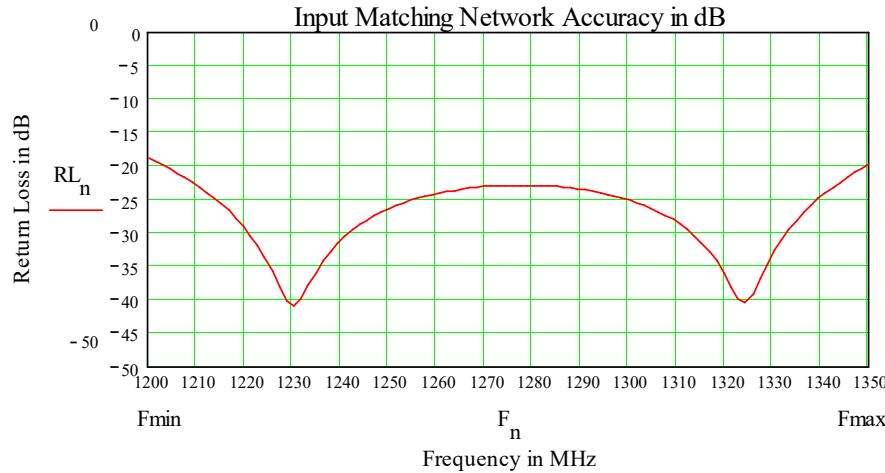
- Network Synthesis using Numerical (iterative) Methods
- Note Lin1 is negative! - Suggests Excessive Package
- Gate Lead Inductance – Small Lin1, Probably Ignore



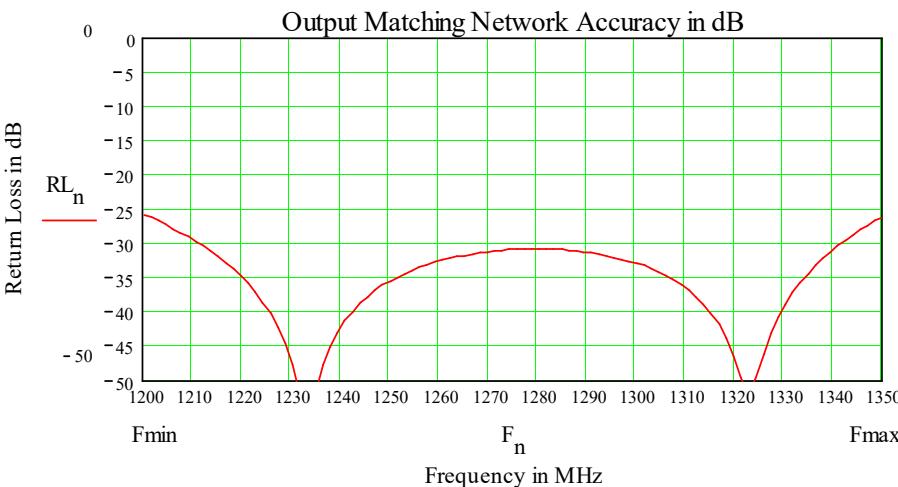
- Prototype LDMOS RFPA with Lumped Element Component Values
- Adequate to Proceed to PCB Microstripline Implementation
- Will Assume Inexpensive FR4

# Field Effect Transistor – FET

## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey



- Note Dual Resonances – Expected for N=4
- Predicted Input Match Better Than -20 dB
- Design Bandwidth Window Should Exceed Required Target (1,200 ~ 1,350 MHz @ -20dB, >> 23 cm band, 1,240 ~1,300 MHz)



- Predicted Output Match Better Than -25 dB
- Design Bandwidth Window Should Exceed Required Target (1,200 ~ 1,350 MHz @ -20dB, >> 23 cm band, 1,240 ~1,300 MHz)

# Field Effect Transistor – FET

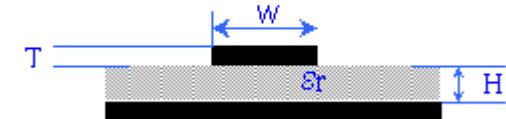
## Chapter 3 - Example RF FET Circuits 3c - 23 cm 15 Watt LDMOS RFPA Design Journey

$$Z_{0\text{pcb}}(\epsilon_r, H, T, W) := \frac{87}{\sqrt{\epsilon_r + 1.41}} \cdot \ln \left( \frac{5.98 \cdot H}{0.8 \cdot W + T} \right)$$

This equation assumes that  $0.1 < W/H < 3.0$  and  $1 < \epsilon_r < 15$ . The corresponding velocity factor VF is approximately equal to  $VF \sim \epsilon_r^{-0.5}$ .

$$w_{\text{eff}} = w + t \frac{1 + \frac{1}{\epsilon_r}}{2\pi} \ln \left( \frac{4e}{\sqrt{\left(\frac{t}{h}\right)^2 + \left(\frac{1}{\pi} \frac{w}{t} + \frac{11}{10}\right)^2}} \right)$$

$$Z_{0\text{pcb2}}(\epsilon_r, H, T, W) := \begin{cases} W_{\text{eff}} \leftarrow W + T \cdot \frac{1 + \frac{1}{\epsilon_r}}{2\pi} \cdot \ln \left[ \frac{4 \cdot e}{\sqrt{\left(\frac{T}{H}\right)^2 + \left(\frac{1}{\pi} \frac{W}{T} + \frac{11}{10}\right)^2}} \right] \\ k \leftarrow 1 + \frac{4 \cdot H}{W_{\text{eff}}} \cdot \left[ \frac{14 + \frac{8}{\epsilon_r}}{11} \cdot \frac{4 \cdot H}{W_{\text{eff}}} + \sqrt{\left( \frac{14 + \frac{8}{\epsilon_r}}{11} \cdot \frac{4 \cdot H}{W_{\text{eff}}} \right)^2 + \pi^2 \cdot \frac{1 + \frac{1}{\epsilon_r}}{2}} \right] \\ \frac{377}{2 \cdot \pi \cdot \sqrt{2 \cdot (1 + \epsilon_r)}} \cdot \ln(k) \end{cases}$$



- Convert Inductors to PCB
- Microstripline, relative permittivity  $\epsilon_r \sim 4.8$ , standard FR4 substrate
- Use substrate height  $H=0.6\text{mm}$
- Track Width  $W \sim 0.8\text{mm}$ ,  $Z_0 = 50\Omega$
- Simple formula for  $Z_0$  applies
- More Complex “Wheeler’s” Formula for Very Wide Tracks

# Field Effect Transistor – FET

**Chapter 3 - Example RF FET Circuits**  
***3c - 23 cm 15 Watt LDMOS RFPA Design Journey***

- Applied RFPA Design Methodology
- Hypothetical 15 Watt 23 cm LDMOS RFPA
- Used PD85015 15 Watt 870 MHz LDMOS Part
- Needed To Extrapolate z-Data to 23 cm
- Prototype Lumped Element Design
- Inductor Conversion to PCB Microstripline

# Field Effect Transistor – FET

- FET Presentation in Three Chapters
- FET History, FET Types, FET Circuits
- Hypothetical 15 Watt LDMOS RFPA

Design for 23 cm, PD85015 870 MHz

- Questions & Comments

# Field Effect Transistor – FET

Inexpensive components, overnight courier – postage waived for orders > \$NZ 125

<http://www.digikey.co.nz/>

Interesting site detailing transistor history – primarily BJT

[http://semiconductormuseum.com/Museum\\_Index.htm](http://semiconductormuseum.com/Museum_Index.htm)

Wikipedia on MOSFET devices – plenty of theory here!

<https://en.wikipedia.org/wiki/MOSFET>

White paper on LDMOS from NXP (ex Philips)

[https://www.nxp.com/files/rf\\_if/doc/white\\_paper/50VRFLDMOSWP.pdf](https://www.nxp.com/files/rf_if/doc/white_paper/50VRFLDMOSWP.pdf)

Internet portal for RF products developed by MACOM

<https://www.macom.com/products/rf-power-products/>

Internet site for Spectrum – free download for Microcap 11 (non commercial use)

<http://www.spectrum-soft.com/index.shtml>

Internet site for “Quite Universal Circuit Simulator” QUCS – free, excellent RF tool

<http://qucs.sourceforge.net/download.html>